Morphology and magnetic properties of a"-Fe₁₆N₂ nanoparticles synthesized from iron hydroxide and iron oxides

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Metastable α "-Fe₁₆N₂ have attracted much interest as a candidate for rare-earth-free hard magnetic materials. To realize high coercivity, it is necessary to utilize not only the magnetocrystalline anisotropy but also the shape anisotropy of α "-Fe₁₆N₂ nanoparticles assemblies. An increase in magnetostatic couplings and intergranular exchange couplings among particles typically reduces the coercivity. Therefore, it is very important to evaluate the anisotropy and magnetic interactions among α "-Fe₁₆N₂ nanoparticles. We have examined the changes in morphology, structure and magnetic properties through the synthesis of α "-Fe₁₆N₂ nanoparticles from various materials such as α -FeOOH, γ -Fe₂O₃, and Fe₃O₄. The magnetic interactions were also estimated based on experimental results obtained by analysis of the rotational hysteresis loss of randomly oriented nanoparticles. H_c and H_k^{ptc} for the α "-Fe₁₆N₂ nanoparticle assemblies for different starting materials ranged from 2.2 to 1.1 kOe, and from 11 to 12 kOe respectively. Experimental results of the normalized coercive force and normalized switching field suggests that the existence of large magnetic interactions among α "-Fe₁₆N₂ nanoparticles.

Key words: nanomagnetics, hard magnetic materials, iron nitride, magnetic anisotropy, rare earth element-free

1. Introduction

The metastable α "-Fe₁₆N₂ iron nitride phase with body-centered tetragonal (b.c.t.) structure has received much attention as a candidate for rare-earth-free hard magnetic materials. After a surprising first report where the a"-Fe16N2 phase exhibited giant saturation magnetization as a thin film¹, many researches have attempted to produce single phase a"-Fe₁₆N_{2^{2,3)}. In 1993,</sub>} a thin film method was established to achieve a relatively high volume fraction of a"-Fe16N2 using reactive sputtering, where a saturation magnetization of $M_s \simeq 240$ emu/g and uniaxial magnetocrystalline anisotropy constant of $K_u \simeq 1 \times 10^7 \text{ erg/cm}^3$ were determined⁴⁾. These values are very attractive with respect to the realization of a permanent magnet based on this material. Since it is still very difficult to produce metastable α "-Fe₁₆N₂ in thin films, the synthesis of single phase a"-Fe16N2 in bulk form is considered to be extremely challenging 5,6,7. In 2013, a procedure for the synthesis of single phase a"-Fe₁₆N₂ nanoparticles was established, and a"-Fe16N2 was reported⁸⁾ to exhibit Ms $\simeq 226$ emu/g and K_u $\simeq 9.6 \times 10^6$ erg/cm³ at 300 K.

To produce a hard magnetic material using magnetic particle, it is necessary to control the anisotropy of particle assemblies and the magnetic interaction among these particles. Magnetostatic couplings and intergranular exchange couplings among particles typically reduce the coercivity. Therefore it is very important to evaluate these magnetic interactions among $\alpha^{"}$ -Fe₁₆N₂ nanoparticles. In this work, we examine the changes in the morphology, structure and magnetic properties of $\alpha^{"}$ -Fe₁₆N₂ nanoparticles synthesized using different starting materials, such as α -FeOOH, κ -Fe₂O₃, and Fe₃O₄. We also discuss the magnetic anisotropy and magnetic interactions based on the experimental results obtained by the rotational hysteresis loss analysis⁹⁾ of randomly oriented nanoparticles.

2. Experimental Procedure

The synthesis of α "-Fe₁₆N₂ nanoparticles was conducted using commercially available a-FeOOH (Wako Pure Chemical Industries, Ltd.), r-Fe₂O₃ (CIK NanoTek Corporation) and Fe₃O₄ (Mitsui Mining & Smelting Co., Ltd.). The diameters of the iron hydroxide and iron oxide particles ranged from several tens to several hundreds of nanometers. The temperature and duration for reduction and nitriding were systematically examined to obtain almost single phase a"-Fe16N2, according to the following procedure. a-FeOOH, r-Fe₂O₃, and Fe₃O₄ nanoparticles were first reduced at 250-600 °C for 1-5 h in a H₂ gas flow. Nitriding was subsequently performed at 100-200 °C for 2-72 h in an NH₃ gas flow. Crystal structure analysis was conducted using powder X-ray diffraction (XRD) with CoKa radiation. Morphological changes were observed using transmission electron microscopy (TEM). For magnetic properties measurements, α -Fe and α "-Fe₁₆N₂ nanoparticles were packed into a disk shape (6 mm diameter, 1 mm thick) with resin. The magnetization σ , and coercivity H_c, were measured using vibrating sample magnetometer (VSM) with a maximum applied magnetic field of 14.5 kOe at 300 K.

3. Results and Discussions

3.1 Morphological and structural changes of nanoparticles prepared from various starting materials

Fig. 1 shows TEM images of α -FeOOH as a starting material, α -Fe produced by the reduction of α -FeOOH, and α "-Fe₁₆N₂ formed by the nitriding of α -Fe. The shape of the Fe hydroxide particles is spindle-like. Reduction was performed in an atmosphere of flowing H₂ at 380 °C for 4 h, and produced aggregates of nanoparticles by sintering. Subsequent nitriding was performed in an atmosphere of flowing NH₃ at 160 °C for 8 h. No morphological differences were observed between the reduced α -Fe and nitrided α "-Fe₁₆N₂ nanoparticle assemblies.

Fig. 2 shows TEM images of the r-Fe₂O₃ starting material, α -Fe reduced from r-Fe₂O₃ and α "-Fe₁₆N₂ as the nitriding product from α -Fe. The shape of the r-Fe₂O₃ particles is spherical. Reduction was conducted in an atmosphere of flowing H₂ at 300 °C for 4 h. The reduction process caused the nanoparticles to form aggregates by sintering, as with the α -FeOOH starting

material. Nitriding was performed in an atmosphere of flowing NH_3 at 145 °C for 8 h. The nitriding process did not result in any morphological changes, in the same way that no changes were observed with the α -FeOOH starting material.

Fig. 3 shows TEM images of the Fe₃O₄ starting material, α -Fe reduced from Fe₃O₄, and α ["]-Fe₁₆N₂ by the nitriding of α -Fe. The shape of the Fe₃O₄ particles is cubic. Reduction was performed in an atmosphere of flowing H₂ at 340 °C for 4 h. The reduction and nitriding processes did not generate any obvious macroscopic morphological changes, in contrast to that observed with the α -FeOOH and γ -Fe₂O₃ starting materials.

Fig. 4 shows representative XRD patterns of the α "-Fe₁₆N₂ nanoparticles produced from various starting materials. In the case of α "-Fe₁₆N₂ nanoparticles produced from α -FeOOH, γ -Fe₂O₃, all X-ray diffracted



Fig.1 TEM images of α -Fe and α "-Fe₁₆N₂ produced from α -FeOOH as a starting material.



Fig. 2 TEM images of α -Fe and α "-Fe₁₆N₂ produced from γ -Fe₂O₃ as a starting material.



Fig. 3 TEM images of α -Fe and α "-Fe₁₆N₂ produced from Fe₃O₄ as a starting material.



Fig. 4 XRD patterns of the α "-Fe₁₆N₂ nanoparticles produced from various starting materials. Asterisks show super-lattice diffraction of N ordered site.

line were identified as $\alpha^{"}$ -Fe₁₆N₂. On the other hand, very small diffracted line besides diffractions of $\alpha^{"}$ -Fe₁₆N₂ observed at diffraction angles around 48 and 99 degrees for $\alpha^{"}$ -Fe₁₆N₂ nanoparticles produced from Fe₃O₄. It is supposed that these additional diffracted line correspond Fe₄N and α -Fe, respectively.

3.2 Shape anisotropy with respect to the agglomeration of nanoparticles

Fig. 5 shows the torque loss curves of α "-Fe₁₆N₂ randomly oriented particle assemblies produced from a-FeOOH changing applying field from 3 to 10 kOe. Rotational hysteresis loss Wr is measured as the region of enclosed these clockwise area by and counterclockwise torque curves. In the case of applying magnetic field H is larger than the half of anisotropy field H_k and smaller than H_k for the randomly oriented particles, rotational hysteresis loss $W_{\rm r}$ is observed and Wr changes as a function of magnetic field⁹⁾. Fig. 6 shows rotational hysteresis loss curves of a-Fe and a"-Fe16N2 nanoparticles assemblies produced from $\alpha\text{-}FeOOH.~H_k{}^{\text{ptc}}$ was defined by plotting W_r versus inverse applied field and finding the intercept by



Fig. 5 Torque loss curves of α "-Fe₁₆N₂ randomly oriented particle assemblies produced from α -FeOOH changing applying field. CW indicates clockwise rotation and CCW indicates counter-clockwise rotation.



Fig. 6 Rotational hysteresis loss curves of α -Fe and α "-Fe₁₆N₂ nanoparticles assemblies produced from α -FeOOH.

linearly extrapolating to zero hysteresis loss. H_p is the magnetic field where W_r reaches its maximum which corresponds to the switching field of assemblies of nanoparticles. H_k^{ptc} and H_p were evaluated with applying magnetic field up to 15 kOe. In the case of assemblies of particles which were magnetically isolated ideally, the value of magnetic field where W_r vanishes is independent of particle alignment (crystallographic orientation) and corresponds to H_k^{ptc} . Similar rotational hysteresis loss analysis had been already applied to the thin film recording media^{10,11}.

Table 1 shows the magnetic properties of α -Fe and α "-Fe₁₆N₂ nanoparticle assemblies produced from the different starting materials, as measured with the VSM and torque magnetometer. M_s for the α -Fe nanoparticle assemblies ranged from 205 to 198 emu/g according to the starting material. Compared to the literature value of the magnetization 218 emu/g for α -Fe, these values are lower from 6 to 9 % than the literature value. It is assumed that oxidation of surface of the α -Fe nanoparticles may cause this decrease in magnetization. H_c for the α -Fe nanoparticle assemblies ranged from 0.8 to 0.3 kOe according to the starting material, and H_k^{ptc}

	α-Fe			α"-Fe ₁₆ N ₂		
Starting material	a-FeOOH	v-Fe ₂ O ₃	$\mathrm{Fe}_{3}\mathrm{O}_{4}$	a-FeOOH	$r - Fe_2O_3$	$\mathrm{Fe}_{3}\mathrm{O}_{4}$
$\mathbf{M_s}$ (emu/g)	205	203	198	226	192	180
$\mathbf{H_{c}}(\mathrm{kOe})$	0.8	0.6	0.3	2.2	1.9	1.1
H_{p} (kOe)	2.0	1.7	1.3	4.2	3.8	3.0
${H_k}^{ptc}$ (kOe)	5.4	6.8	7.2	12.0	11.0	11.3
ΔN^{ptc}	3.3	4.3	4.6			
Aspect ratio *	2.2	3.0	3.5			

Table 1. Magnetic properties of α -Fe and α "-Fe₁₆N₂ nanoparticle assembliesproduced from various starting materials.

* Equivalent aspect ratio as nanoparticle assemblies

for the α -Fe nanoparticle assemblies also ranged from 5.4 to 7.2 kOe. For α -Fe nanoparticle assemblies, the anisotropy field H_k^{ptc} is considered to be due to the shape anisotropy of the nanoparticle assemblies because the magnetocrystalline anisotropy constant K_1 for α -Fe with cubic symmetry is too small (ca. 1×10⁵ erg/cm³). It is considered that the differences of H_k^{ptc} are derived from the difference of shape anisotropy in the assemblies of α -Fe nanoparticles that are formed during the reduction process. H_c for the α -Fe nanoparticle assemblies decreased from 0.8 to 0.3 kOe even though H_k^{ptc} of them increased from 5.4 to 7.2 kOe. It is assumed that H_c is not determined by only shape anisotropy. Further detailed investigation is necessary to reveal the factor which affects H_c of α -Fe.

Shape anisotropy is expressed as $K_u{}^{shape} = \Delta N \cdot M_s{}^{2/2}$ (or $H_k{}^{shape}{=}\Delta N \cdot M_s$). ΔN is the difference of the demagnetization coefficients between the long and short axes of a particle. The experimentally determined $H_k{}^{ptc}$ was used to estimate ΔN^{ptc} as an equivalent demagnetization coefficients as nanoparticle assemblies. Fig. 7 shows an example of the calculated result^{12} for



Fig. 7 Shape anisotropy field as a function of the aspect ratio for the ellipsoid form.

 H_k^{shape} as a function of the aspect ratio, assuming an ellipsoid form and that the M_s of α -Fe is 218 emu/g. In this way, the values of ΔN^{ptc} were determined to range from 3.3 to 4.6 for the corresponding aspect ratios of α -Fe nanoparticle assemblies estimated with this scheme, from 2.2 to 3.5. As shown in Fig. 7, the maximum shape anisotropy is expected to be 8×10^6 erg/cm³ with a high aspect ratio of more than 50 which is considered to be very difficult to realize.

On the other hand, H_c for the α "-Fe₁₆N₂ nanoparticle assemblies ranged from 2.2 to 1.1 kOe for different starting materials. The reason why that H_c of α "-Fe₁₆N₂ nanoparticles which were produced from Fe₃O₄ is lower than those of a"-Fe16N2 nanoparticles which were produced from a-FeOOH and x-Fe₂O₃ is considered due to the additional a-Fe which was observed in X-ray diffraction(Fig. 4). H_k^{ptc} for the α "-Fe₁₆N₂ nanoparticle assemblies were not significantly different, ranging from 11 to 12 kOe. The magnetocrystalline anisotropy field H_k^{int} of α "-Fe₁₆N₂ determined for a pseudo single -crystalline film was 11.2 $kOe^{13)}\!.$ This $H_k{}^{ptc}$ for the a"-Fe16N2 nanoparticle assemblies are almost equal to H_k^{int} . If we assume α "-Fe₁₆N₂ nanoparticle assemblies have the same magnetocrystalline anisotropy field H_k^{int} of a pseudo single-crystalline film, the shape anisotropy is considered to be very small in $\alpha^{"}\mbox{-}\mbox{Fe}_{16}N_2$ nanoparticle assemblies.

3.3 Evaluation of magnetic interaction among $\alpha^{"}$ -Fe₁₆N₂ nanoparticle assemblies

Fig. 8 shows plots of the normalized coercive force (H_c/H_k^{ptc}) versus normalized switching field (H_p/H_k^{ptc}) for a"-Fe₁₆N₂ nanoparticle assemblies produced from the various starting materials. H_c/H_k^{ptc} varied from 0.10 to 0.26 and H_p/H_k^{ptc} varied from 0.26 to 0.35. In the ideal magnetization reversal mode due to the coherent rotation of the magnetic moment with nonmagnetic interaction (Stoner-Wohlfarth type)¹⁴⁾, H_c/H_k^{ptc} is equal to 0.48 and H_p/H_k^{ptc} is equal to 0.51. According to the micromagnetic simulation, and it was demonstrated



Fig. 8 Plots of H_c/H_k^{ptc} and H_p/H_k^{ptc} for α "-Fe₁₆N₂ nanoparticles prepared from various starting materials.

that both H_c and H_p decrease with increasing magnetic interaction among grains in thin film media^{11)}. Compared to the ideal values of $H_c/H_k{}^{\rm ptc}$ and $H_p/H_k{}^{\rm ptc}$, these values of $\alpha^{"}\cdot Fe_{16}N_2$ nanoparticles prepared from various starting materials are relatively small. To increase the coercivity of $\alpha^{"}\cdot Fe_{16}N_2$ nanoparticles, it is necessary to decrease magnetic interaction.

3.4 Toward an increase in the coercivity of α "-Fe₁₆N₂ nanoparticle assemblies

The empirical figure known as the magnetic hardness parameter $\kappa = (K_1/\mu_0 M_s^2)^{1/2}$ is a useful parameter to consider how to approach the construction of modern permanent magnet¹⁵. The κ value for Nd₂Fe₁₄B as a typical modern magnet, is 1.54, while that for α "-Fe₁₆N₂ is 0.53. It is recommended that κ be greater than 1, which corresponds to a value of $K_1 \approx$ 3×10^7 erg/cm³, assuming the same magnetization of Nd₂Fe₁₄B, 165 emu/g. The expected shape anisotropy is in the order of 10⁶ erg/cm³ for α "-Fe₁₆N₂ nanoparticles even though a high aspect ratio is realized (Fig. 7); therefor, magnetocrystalline anisotropy in the order of 10^7 erg/cm³ is still required, in addition to improvement of the magnetic isolation among nanoparticles, for application as a permanent magnets.

4. Conclusion

The structural and magnetic properties of α "-Fe₁₆N₂ nanoparticles synthesized from different starting materials were examined, and the magnetic anisotropy of nanoparticle assemblies and magnetic interactions among nanoparticles were evaluated by rotational hysteresis loss analysis.

1. α -Fe nanoparticle assemblies produced by reduction and nitriding of different starting materials show exhibited different values of H_k^{ptc} ranging from 5.4 to 7.2 kOe. It is considered that the differences of H_k^{ptc} are derived from the difference of shape anisotropy in the assemblies of α -Fe nanoparticles that are formed during the reduction process. From these H_k^{ptc} values, the aspect ratio of α -Fe nanoparticle assemblies were estimated to be in the range of 2.2-3.5.

2. H_c for the α "-Fe₁₆N₂ nanoparticle assemblies ranged 2.2 to 1.1 kOe for different starting materials. H_k^{ptc} for the α "-Fe₁₆N₂ nanoparticle assemblies were not significantly different, ranging from 11 to 12 kOe.

3. The normalized coercive force (H_c/H_k^{ptc}) and normalized switching field (H_p/H_k^{ptc}) are 0.10-0.26 and 0.26-0.35 respectively, which indicates large magnetic interactions.

4. As the expected shape anisotropy is in the order of 10^6 erg/cm^3 for a"-Fe₁₆N₂ nanoparticles even though a high aspect ratio is realized, magnetocrystalline anisotropy on the order of 10^7 erg/cm^3 is still required, in addition to improvement of the magnetic isolation among nanoparticles to realize a permanent magnet.

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References

- 1) T. K. Kim, M. Takahashi: *Appl. Phys. Lett.*, **20**, 492 (1972)
- 2) J. M. D. Coey, K. O'Donnell, Q. Qinian, E. Touchais, K. H. Jack: J. Phys.: Condens. Matter, 6, L23 (1994).
- 3) M. Komuro, Y. Kozono, M. Hanazono, and Y. Sugita: J. Appl. Phys. 67, 5126 (1990)
- M. Takahashi, H. Shoji, H. Takahashi, T. Wakiyama: *IEEE Trans. Magn.*, 29, 3040 (1993).
- M. Takahashi, H. Shoji: J. Magn. Magn. Mater. 208, 145 (2000).
- E. Kita, K. Shibata, H. Yanagihara, Y. Sasaki, M. Kishimoto: J. Magn. Magn. Mater., 310, 2411 (2007).
- S. Kikkawa, A. Yamada, Y. Masubuchi, T. Takeda: *Mater. Res. Bull.*, 43, 3352 (2008).
- 8) T. Ogawa, Y. Ogata, R Gallage, N. Kobayashi, N Hayashi, Y Kusano, S. Yamamoto, K. Kohara, M. Doi, M. Takano, M Takahashi: *Appl. Phys. Express*, 6, 073007 (2013).
- 9) I. S. Jacobs, F. E. Luborsky: J. Appl. Phys., 28, 467 (1957).
- 10) M. Takahashi, T. Shimatsu, M. Suekane, M. Miyamura, K. Yamaguchi, H. Yamasaki: *IEEE Trans. Magn.*, 28, 3285 (1992).
- I. A. Beardsley and V.S. Speriosu: *IEEE Trans. Magn.*, 26, 2718 (1990).
- 12) R. C. O'Handley, Modern Magnetic Materials: Principle and Applications, 1st ed. (John Wiley & Sons, Inc., New York, 1999), pp.38-43.
- 13) M. Takahashi, Y. Takahashi, K. Sunaga, H. Shoji: J. Magn. Magn. Mater., 239, 479 (2002).
- 14) E. C. Stoner, E. P. A. Wohlfarth: *Phil. Trans. R. Soc. Lond.*, A 240, 599 (1948).
- 15) R. Skomski, J. M. D. Coey: Scripta Materialia, 112, 3 (2016)

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